

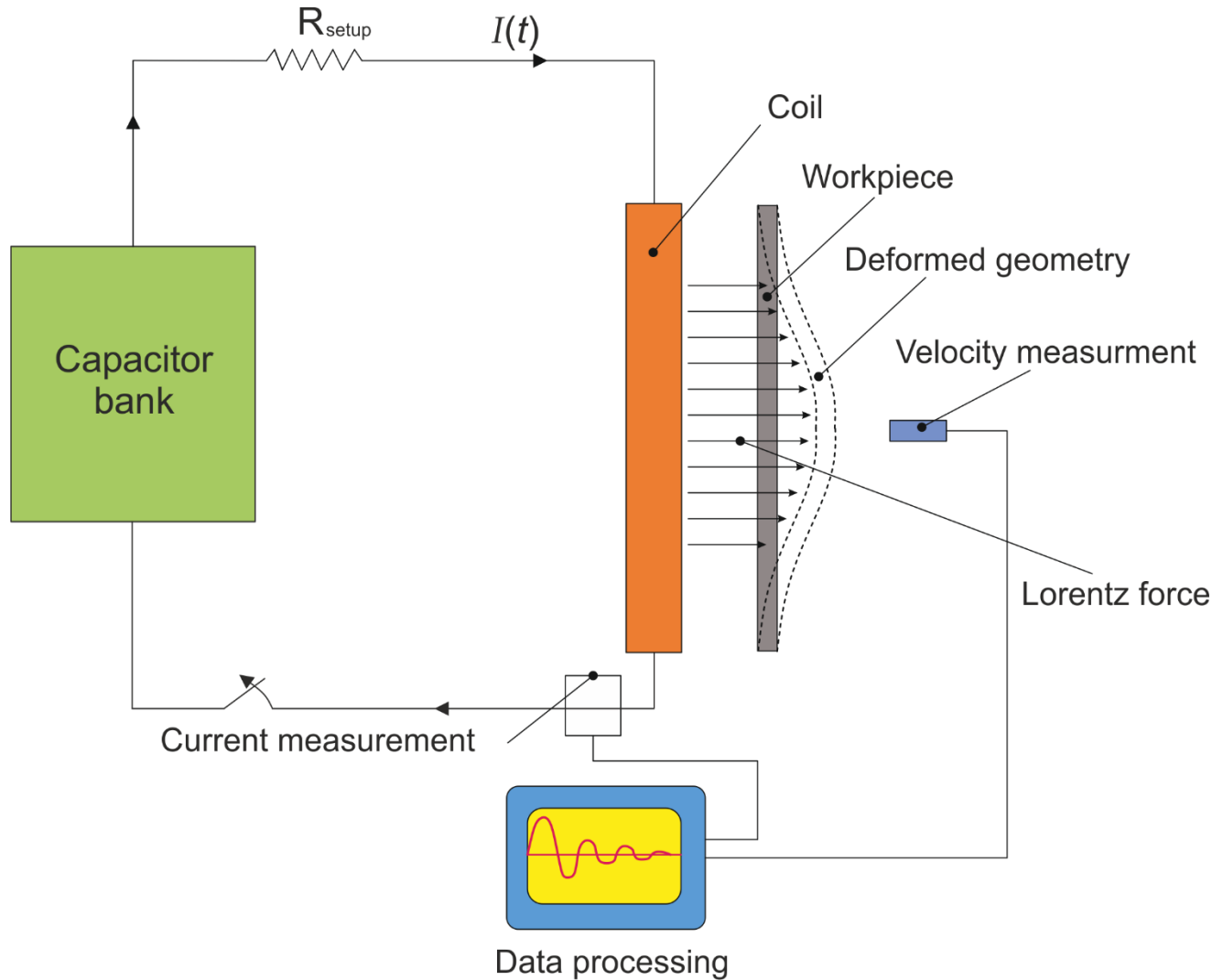


Analytical-based modeling for electromagnetic sheet metal forming with multi-turn coils

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- Introduction
- Objective
- Semi-analytical model
 - Development
 - Validation
- Conclusion

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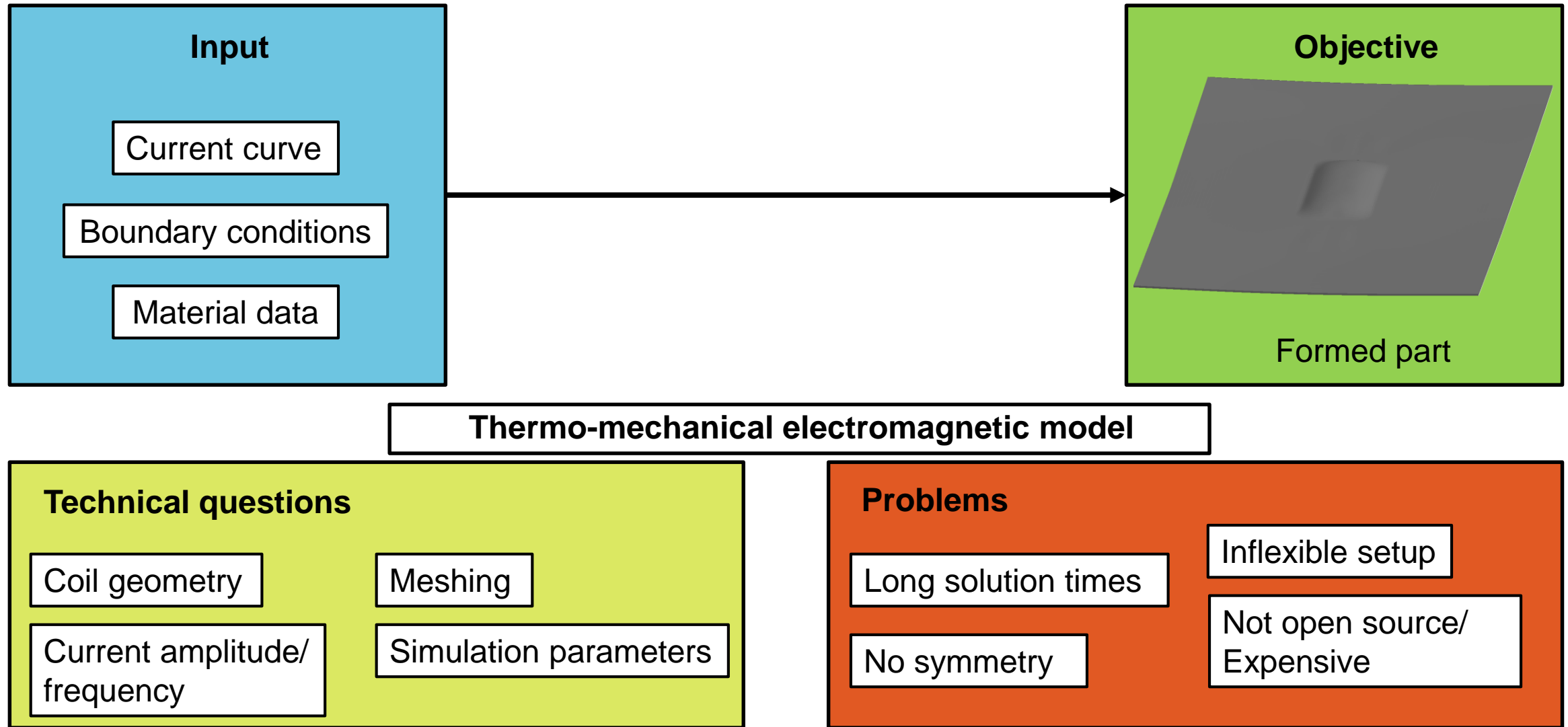
Electromagnetic forming (EMU) of sheet metal

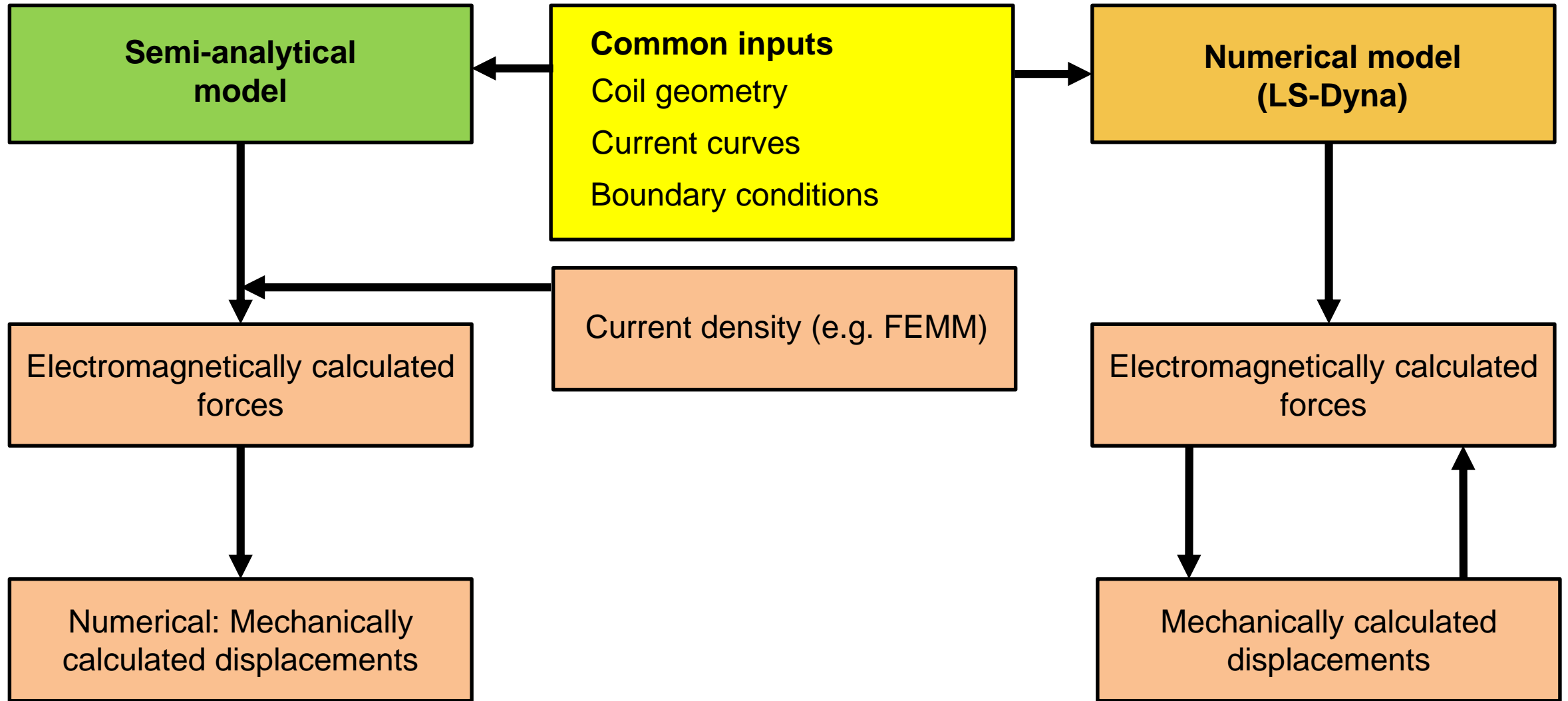
Research areas

- Prediction of the workpiece geometry after the forming process
- Design of the coil (tool) to increase tool life
- Optimization of different process parameters

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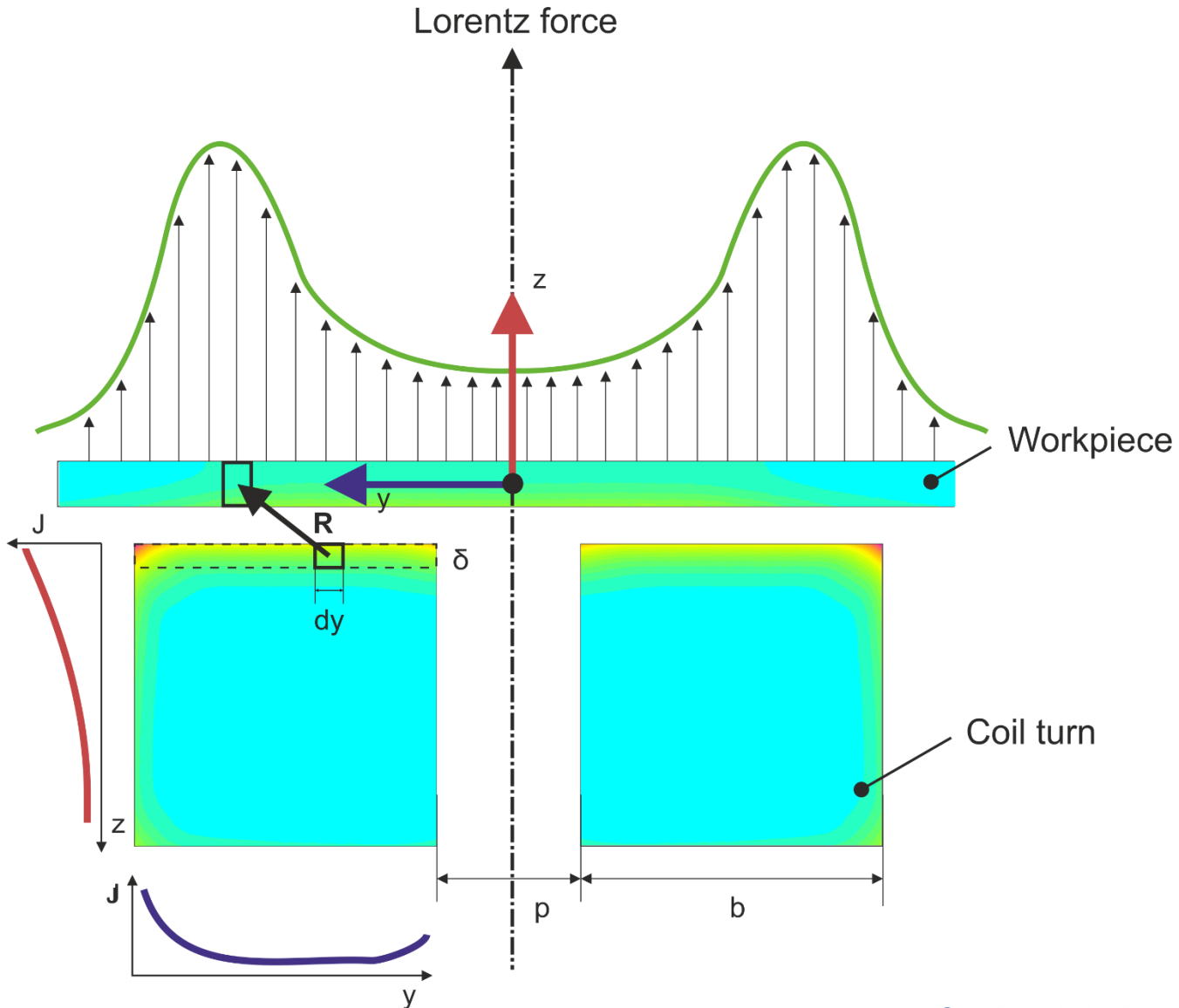
Disadvantages of the current numerical approach (LS-Dyna/FEM+BEM)





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Assumptions of the model

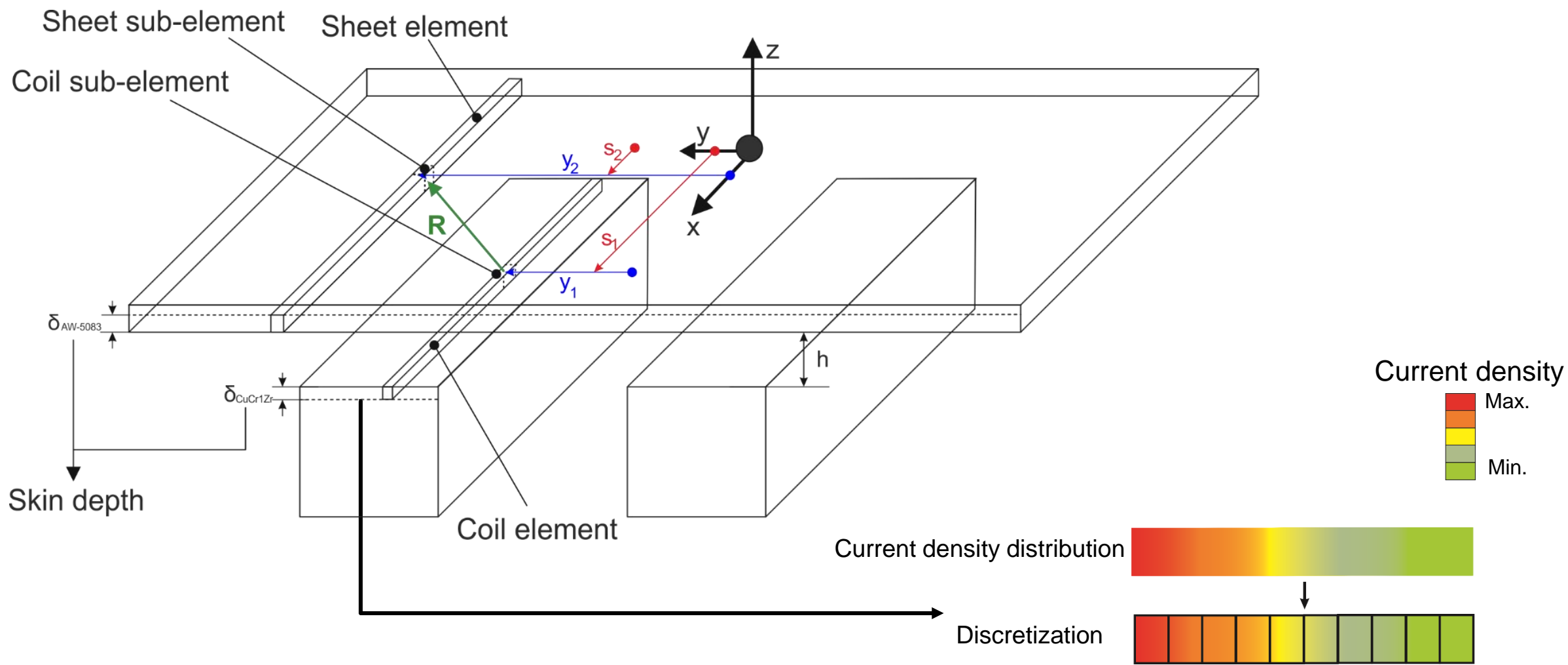


Assumptions

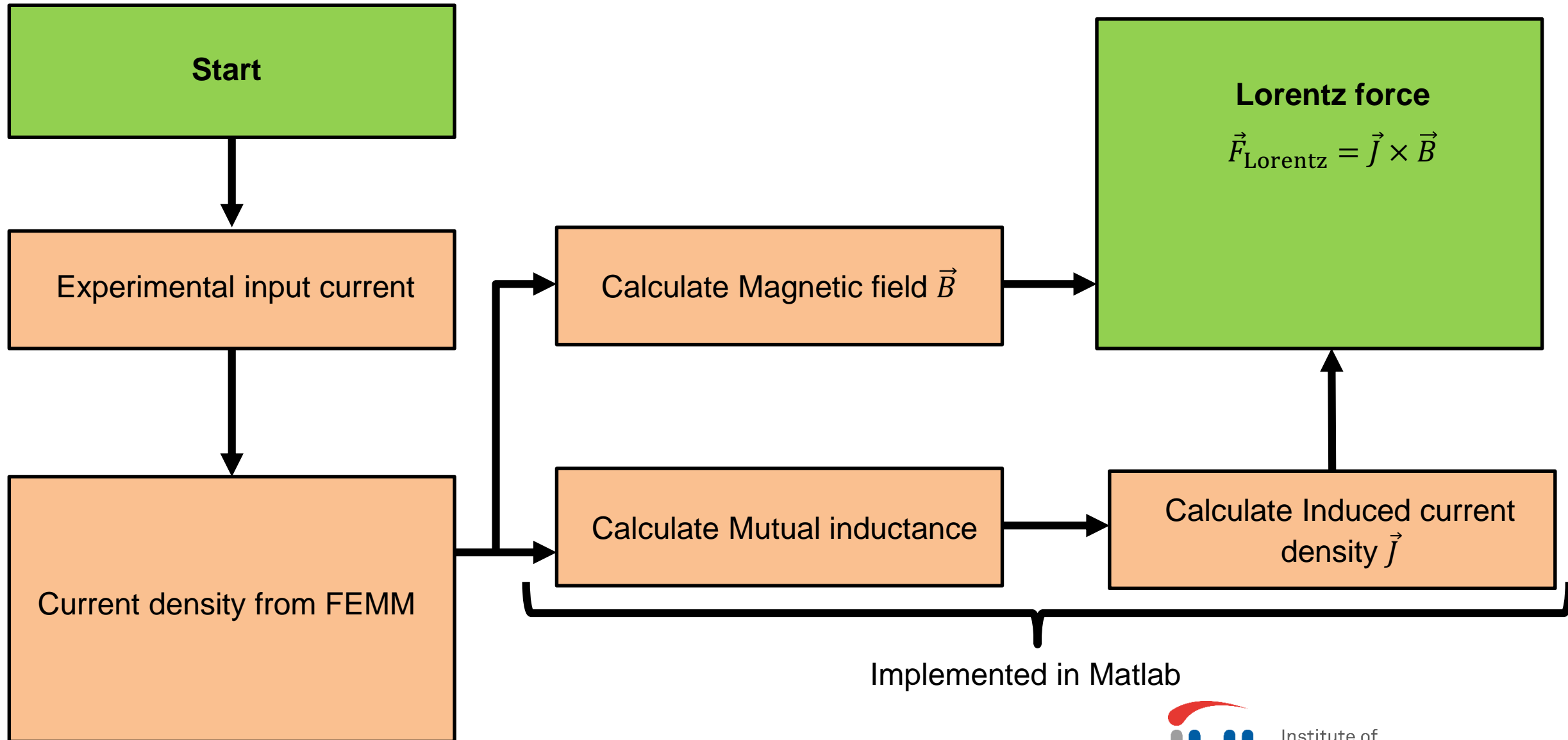
- No displacement of the workpiece
- All current flows in the upper layer
- Current density variation only in y-direction - $J(y)$
- No temperature changes

Semi-analytical model

Structure of the model



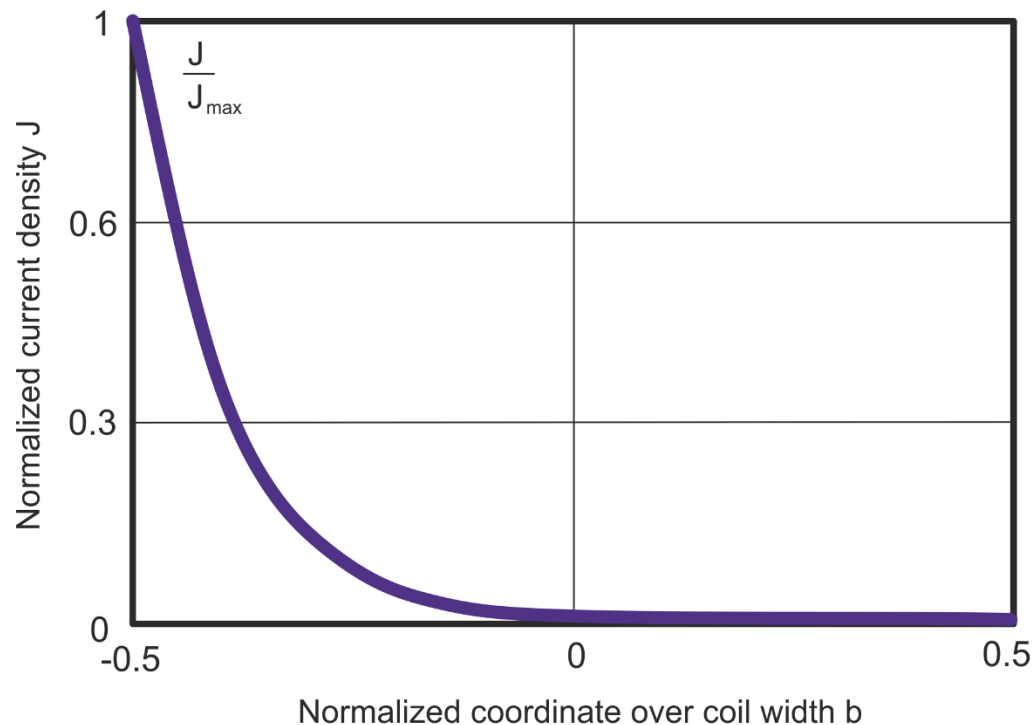
Semi-analytical calculation procedure



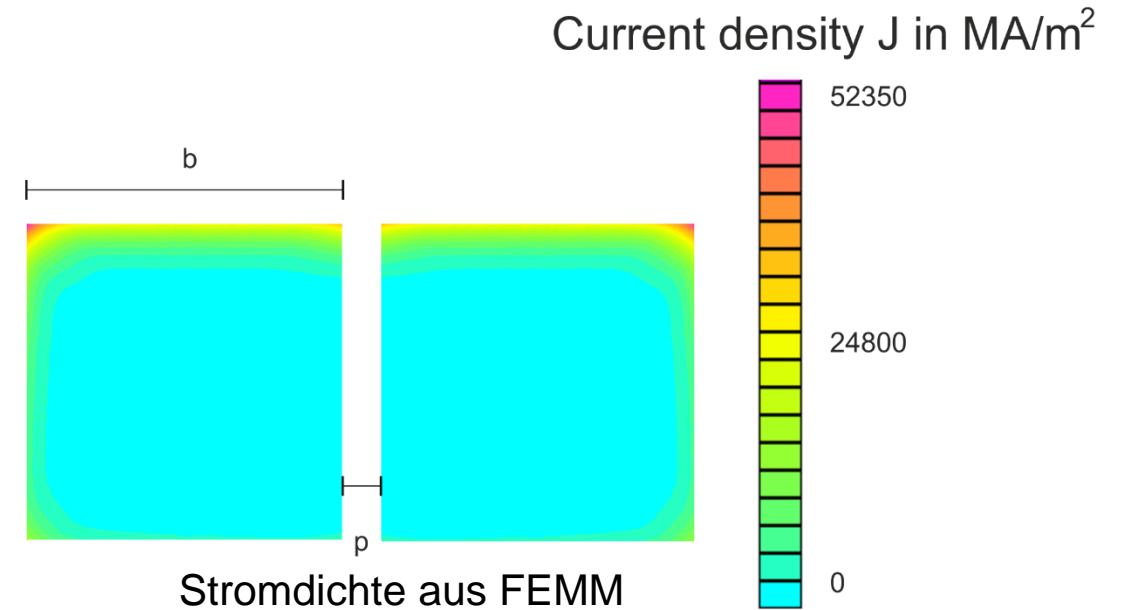
Current density distribution in the coil

Influencing parameters

- Distance between coil turns (p)
- Skin effect
- Electrical conductivity
- Shape of the cross section



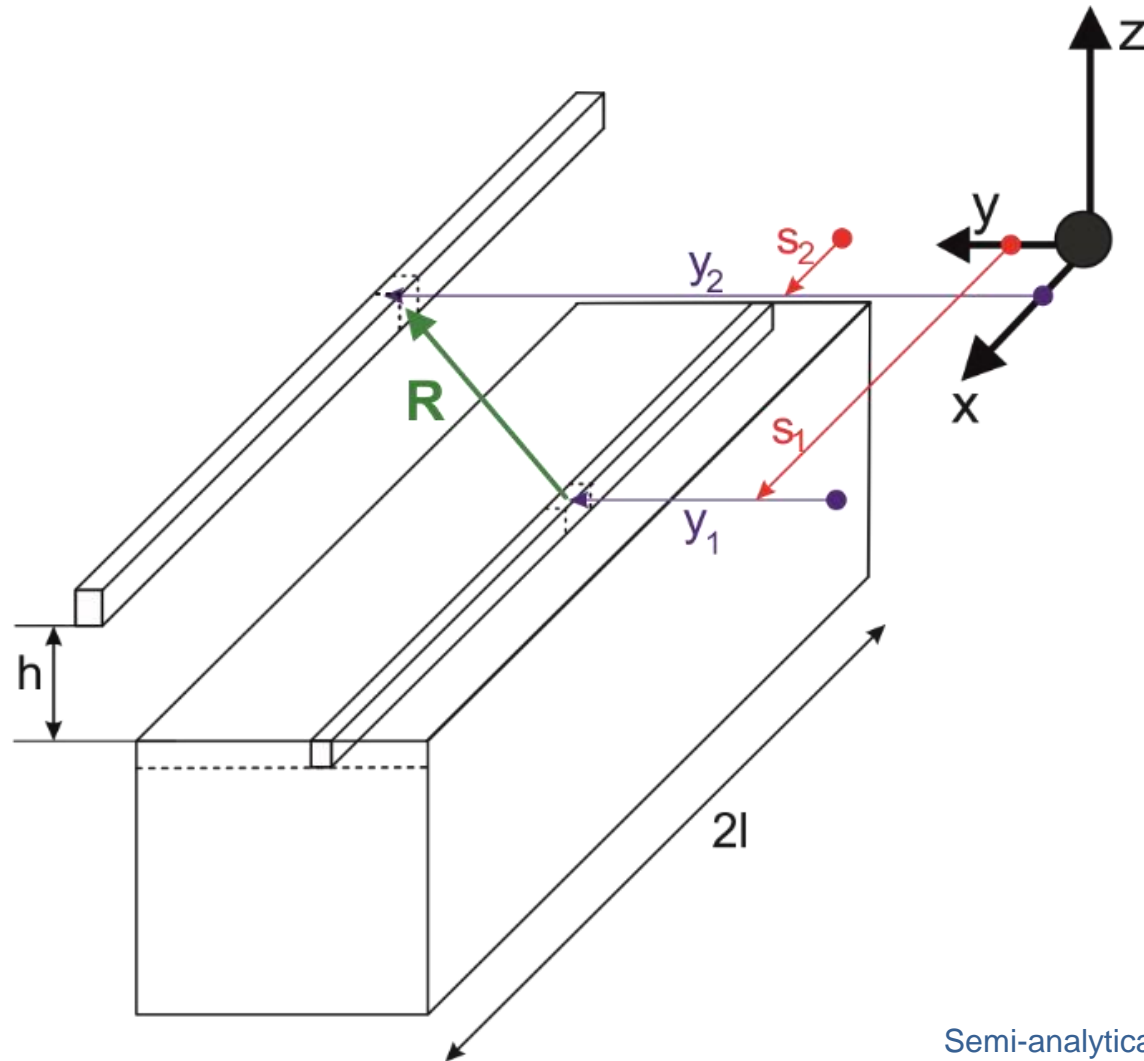
Source: Adelbagi, 2007



- Previous analytical models ignore the proximity effect
- Only for very simple cross sections (rectangular, circular)

Mutual Inductance

Interaction between the magnetic field of two electrical conductors



$$L_{12} = \frac{\mu_0}{4\pi} \oint_{C_1} \oint_{C_2} \frac{\mathbf{ds}_1 \cdot \mathbf{ds}_2}{R}$$

Here:
$$L_{12} = \frac{\mu_0}{2\pi} \left[l \sinh^{-1} \left(\frac{l}{b} \right) + b - \sqrt{l^2 + b^2} \right]$$

$$b = \sqrt{(y_2 - y_1)^2 + h^2}$$

Induced Potential difference (V)

$$V = -L_{12} \frac{dI_1}{dt}$$

Here, I_1 is the input current

Induction current

Induced current paths are known

Resistance (R_e) of an element

$$R_e = \frac{l}{\sigma A}$$

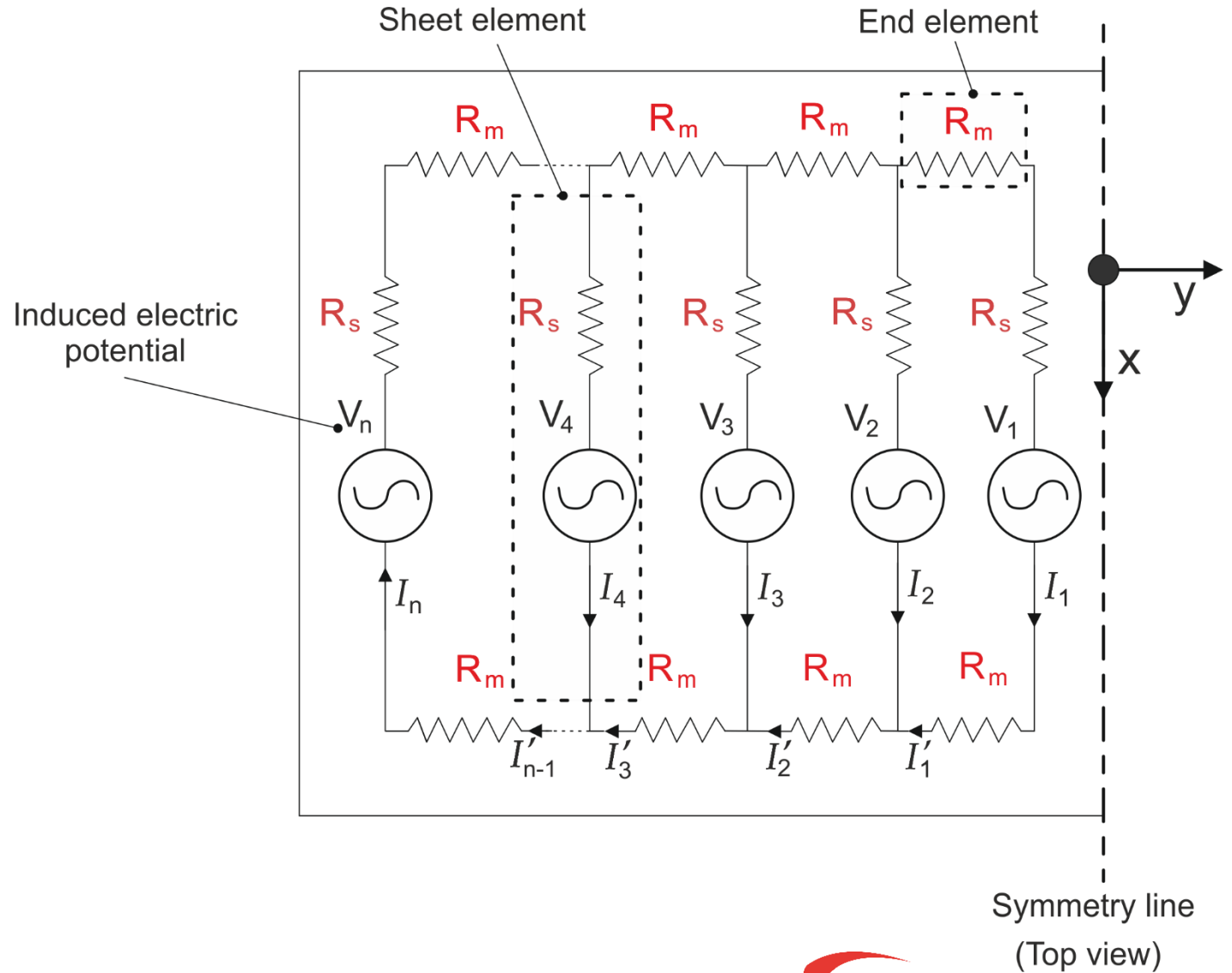
l - Element length

A - Cross-sectional area of the element

σ - Electrical conductivity

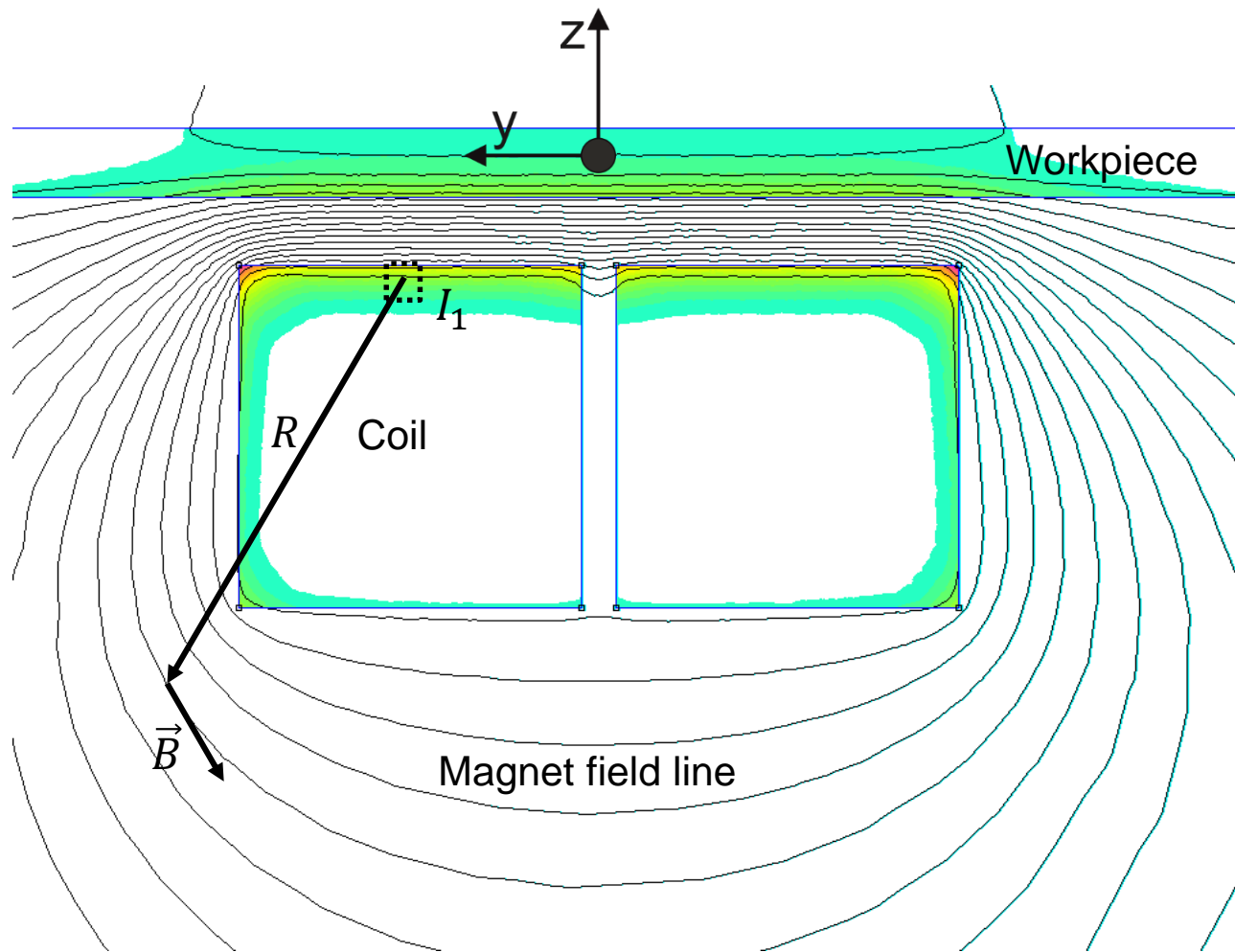
From Ohm's law

$$[V_s] = [V] - R_s[I]$$



Magnetic field (\vec{B})

Calculation based on the current with Biot-Savart's law



Semi-analytical model

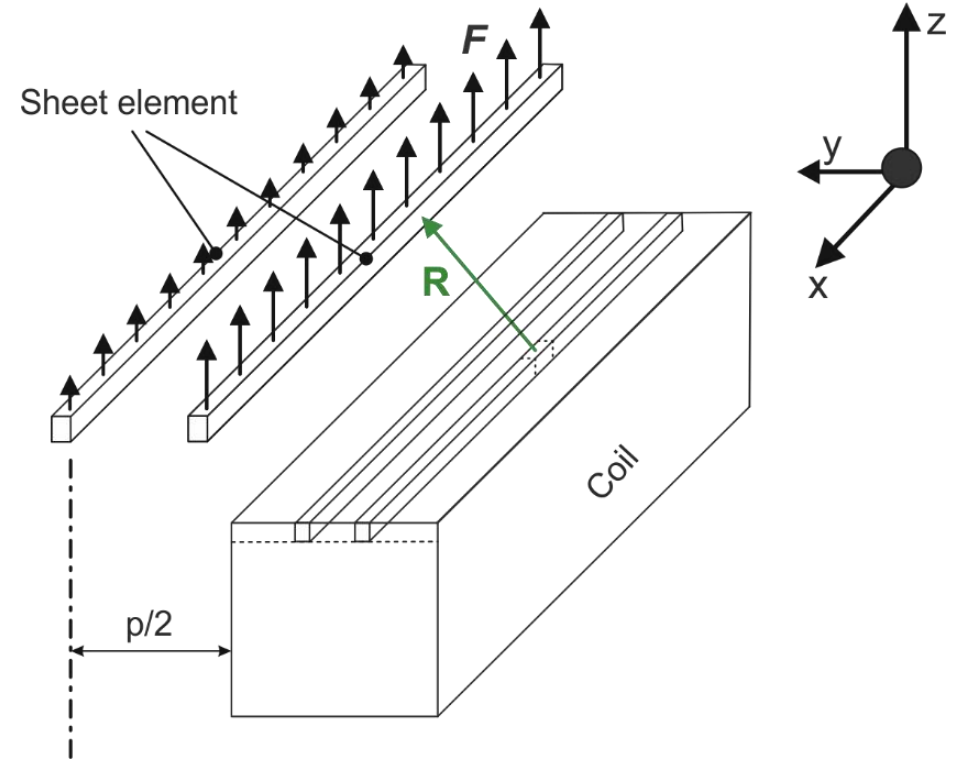
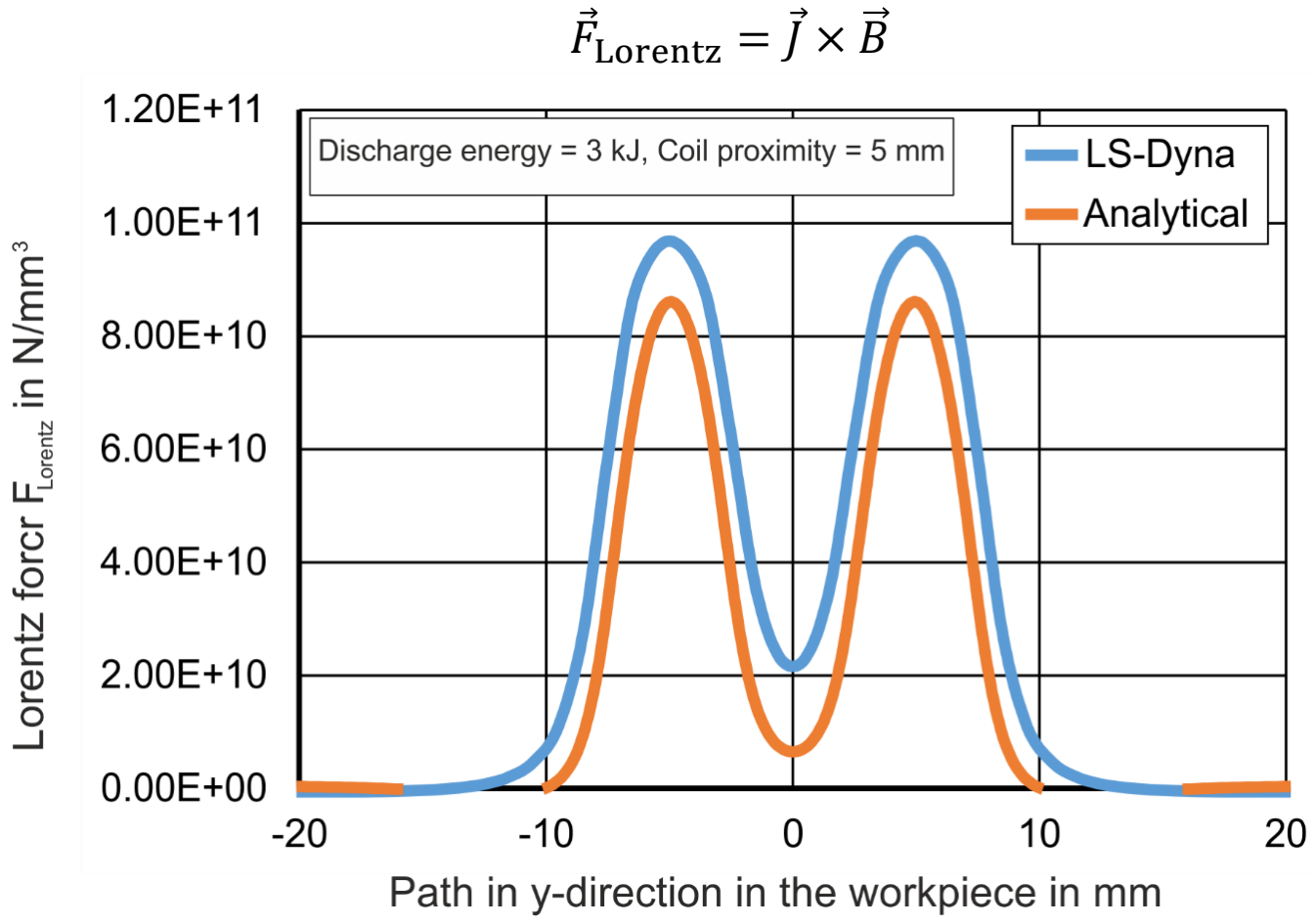
Biot-Savart's law

$$\vec{B} = \frac{\mu_0 I_1}{4\pi} \oint_{C_1} \frac{d\mathbf{s} \times \mathbf{R}}{R^3}$$

Here:

$$\vec{B}_y = \frac{\mu_0 I_1}{4\pi} \left[\frac{\frac{l}{2} - s_2}{b^3 \sqrt{\frac{(\frac{l}{2} - s_2)^2}{b^2} + 1}} \right] - \left[\frac{-\frac{l}{2} - s_2}{b^3 \sqrt{\frac{(-\frac{l}{2} - s_2)^2}{b^2} + 1}} \right]$$

Lorentz force distribution in the workpiece



Time-dependent input current

$$I = I_0 e^{-\lambda t} \sin \omega t$$

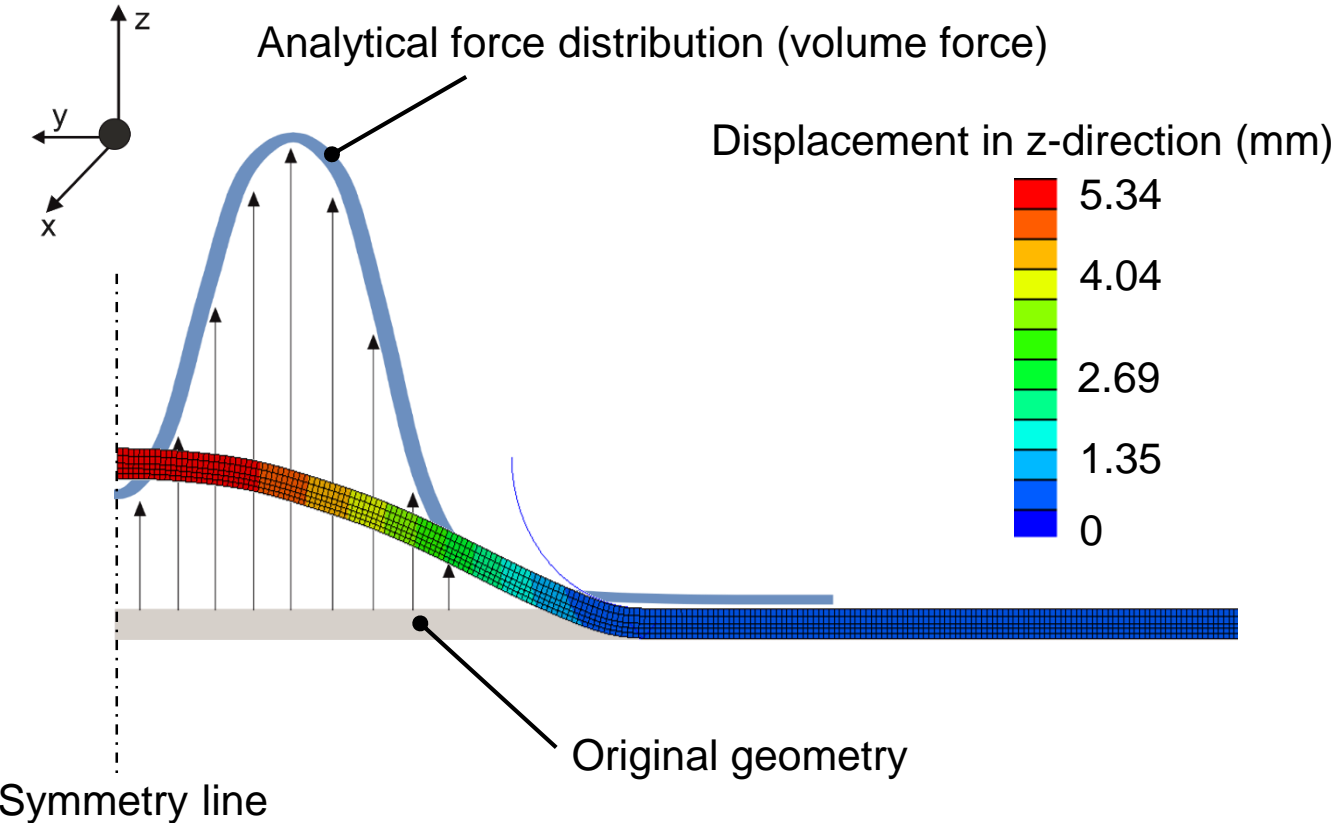
Time dependent force

$$F = F_0 e^{-2\lambda t} \sin^2 \omega t$$

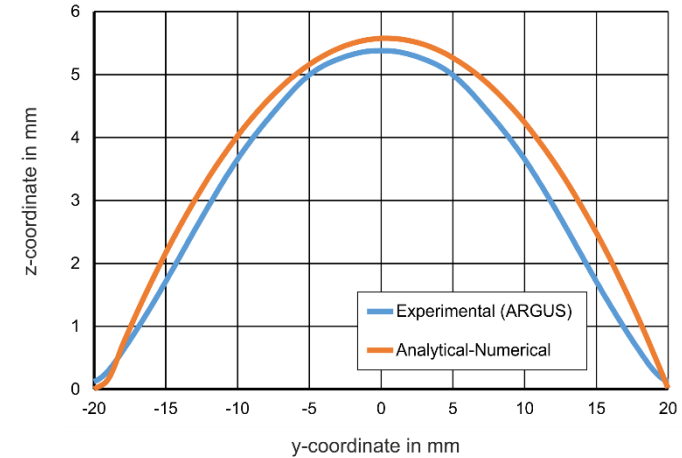
Results and validation

Simulation for validation in ABAQUS

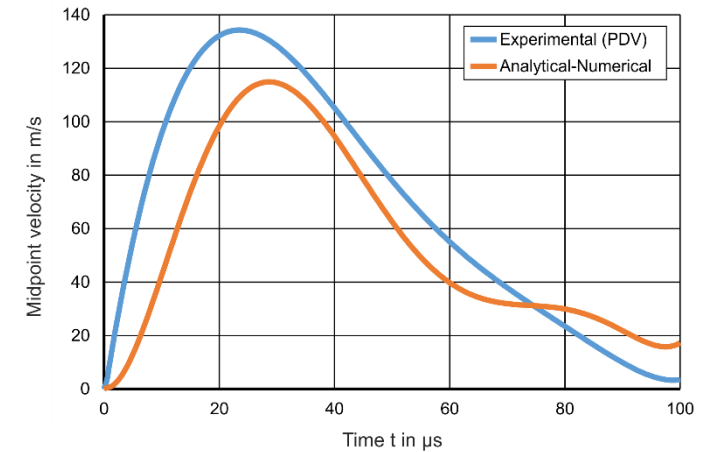
Discharge energy = 3 kJ, Coil proximity = 5 mm



Comparison of the final workpiece geometries



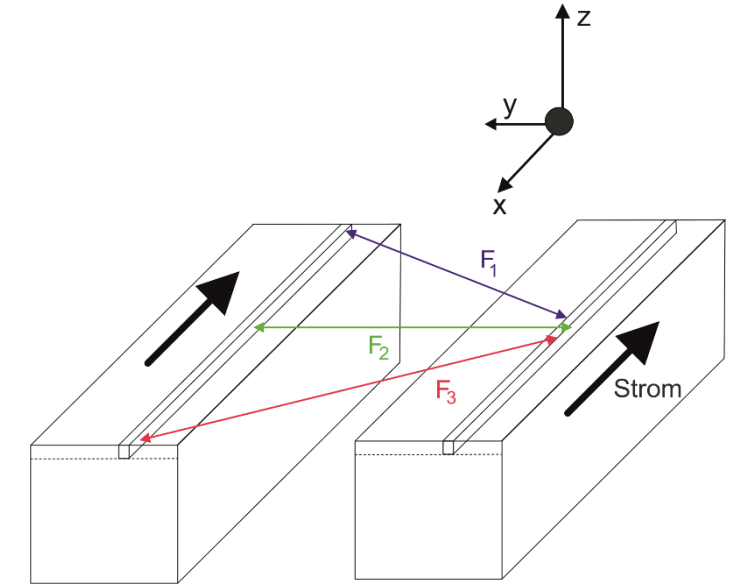
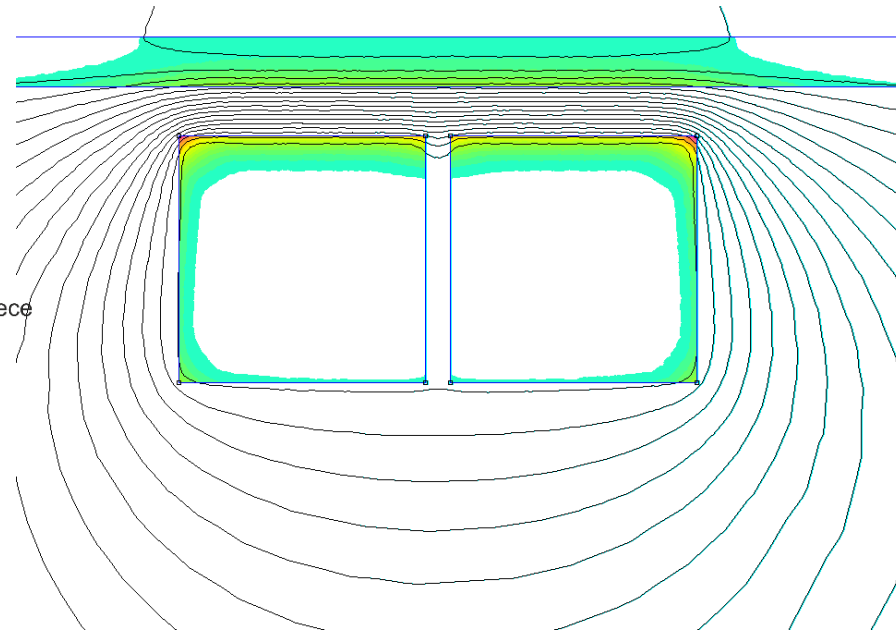
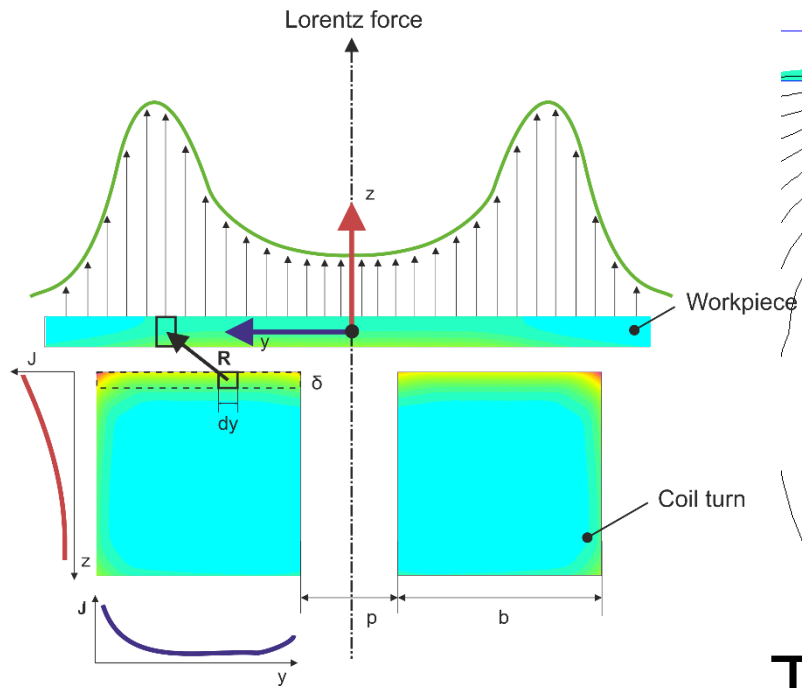
Comparison of midpoint velocities



Quelle: Kabirian et al., 2014

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- Development of a semi-analytical model, without additional time needed to solve multiple coil turns
- Use of numerical current density distribution unavoidable
- LS-Dyna modeling replaceable for some cases



Thank you for your attention