



# Separating the roles of speed, strain-rate and shock in interpreting dynamic hardness

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# Outline

- Introduction of dynamic hardness
- Hardening phenomenal and existing mechanism
- Simulation approach and results
- Discussion on shock hardening
- Summary and future work



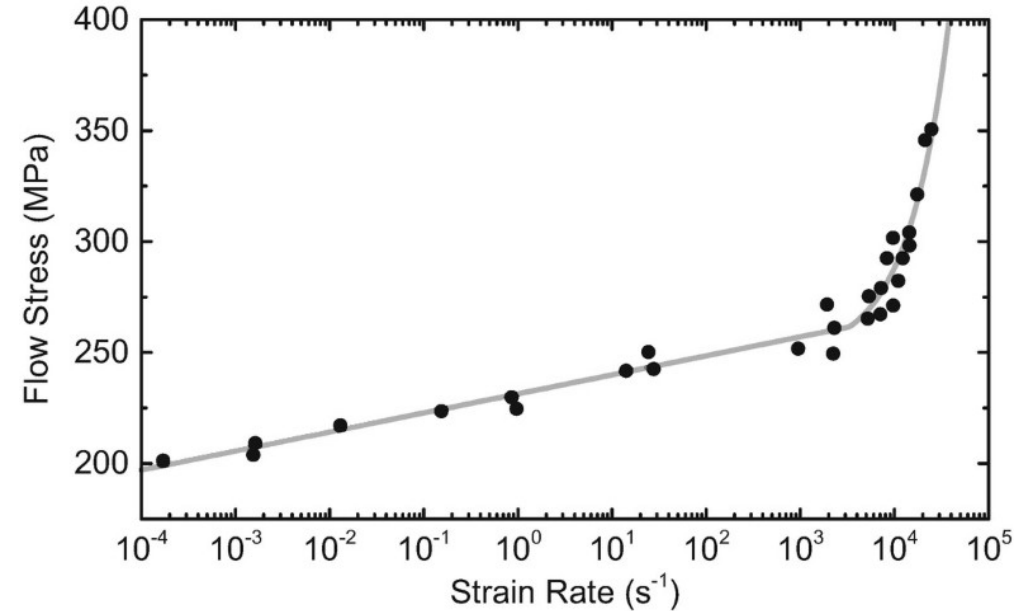
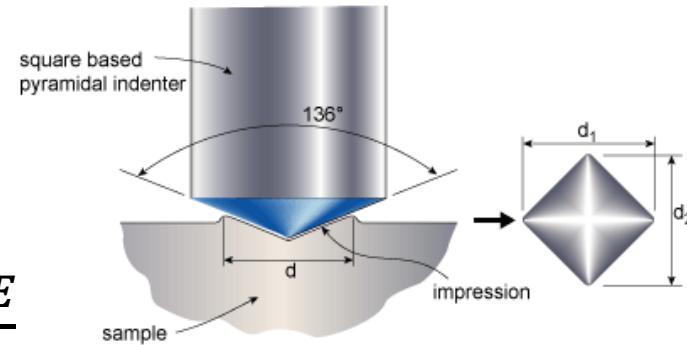
# Dynamic hardness: introduction

- Metal behavior changes dramatically at high strain rate vs static.

- Static hardness:  $H_s = \frac{P}{S}$

- Hardness ratio:  $R_H = \frac{H}{\sigma_y}$

- Dynamic hardness:  $H_d = \frac{E}{V}$



Follansbee et al., 1984

$$H_d = \begin{cases} \frac{\Delta E_k}{V_{indentation}} =, \text{ for dynamic projectile} \\ \frac{\Delta E_p}{V_{indentation}} , \text{ for static load and indentation} \end{cases}$$

Slip-line field theory:  $R_H = 2.96$

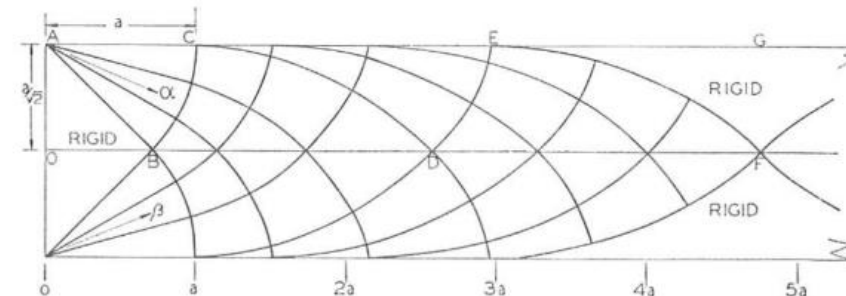
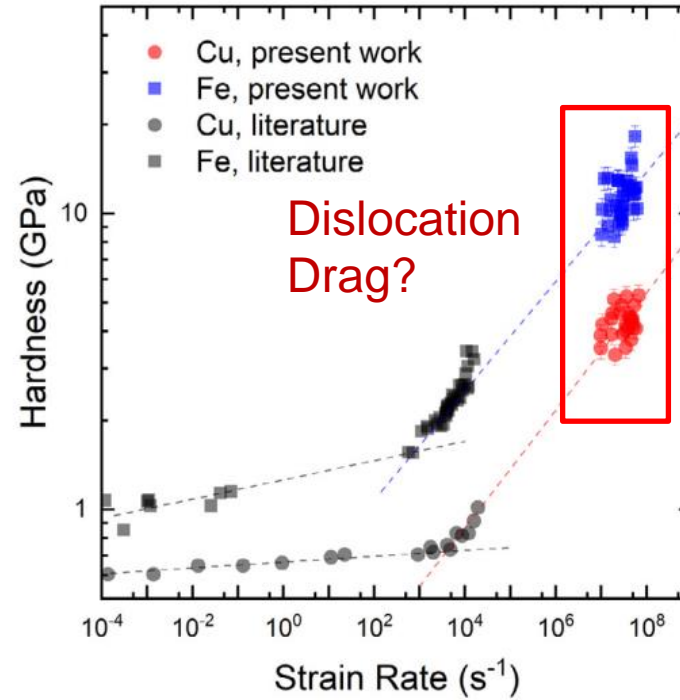
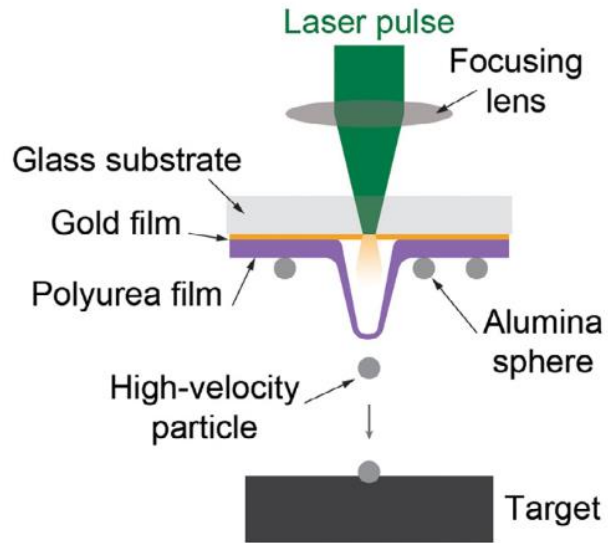


FIG. 7 SHOWING SLIP-LINE FIELD TO SCALE FOR BLOCK OF LENGTH-HEIGHT RATIO 6.72 AT INTERVALS OF 15 DEG IN  $\phi$

Hill et al., 1951



# Dynamic hardness: mechanism debate



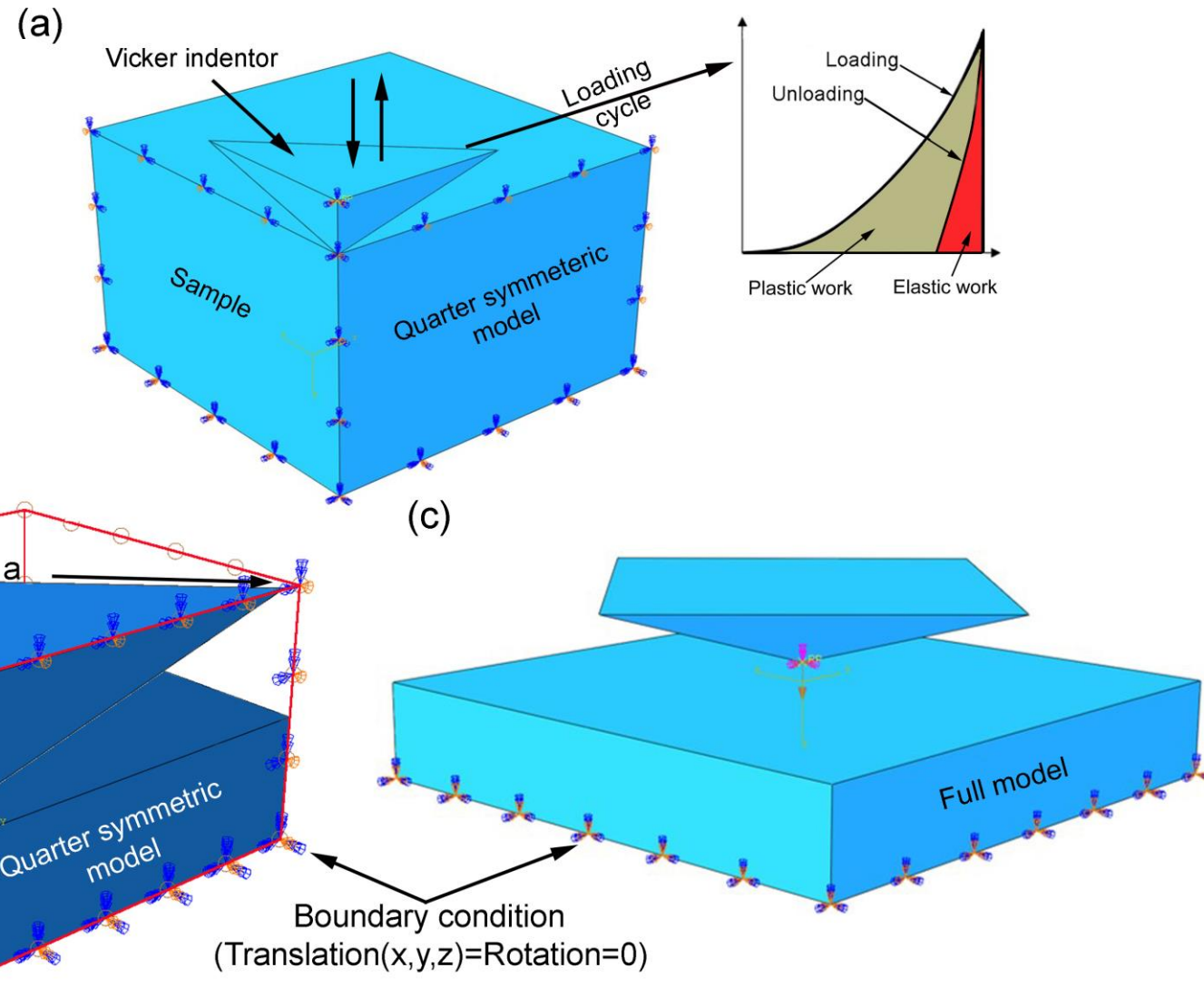
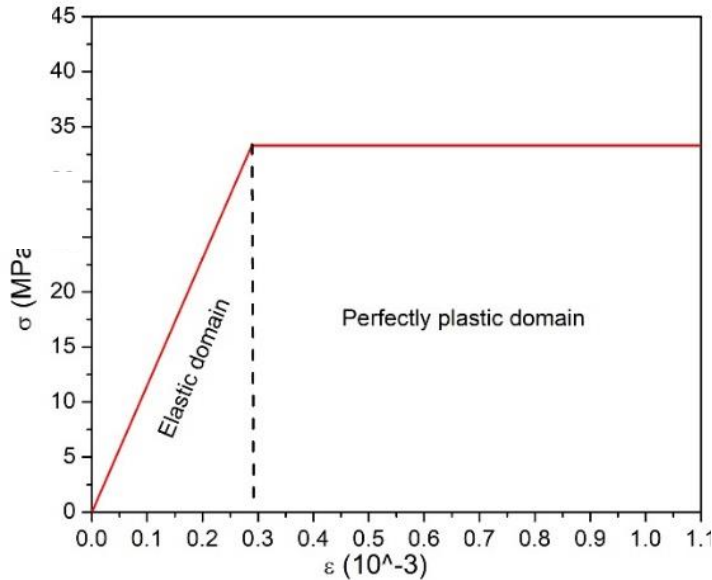
- Dynamic hardness of 10 times of static hardness is obtained at strain rate of  $10^6 s^{-1}$
- High ratio strength increase suggested to be Dislocation Drag.

$$Hardness = \frac{W_{plastic}}{V_{indentation}} = \frac{(1/2) \times m_p \times (v_i^2 - v_r^2)}{V_{indentation}}$$

# Simulation setup

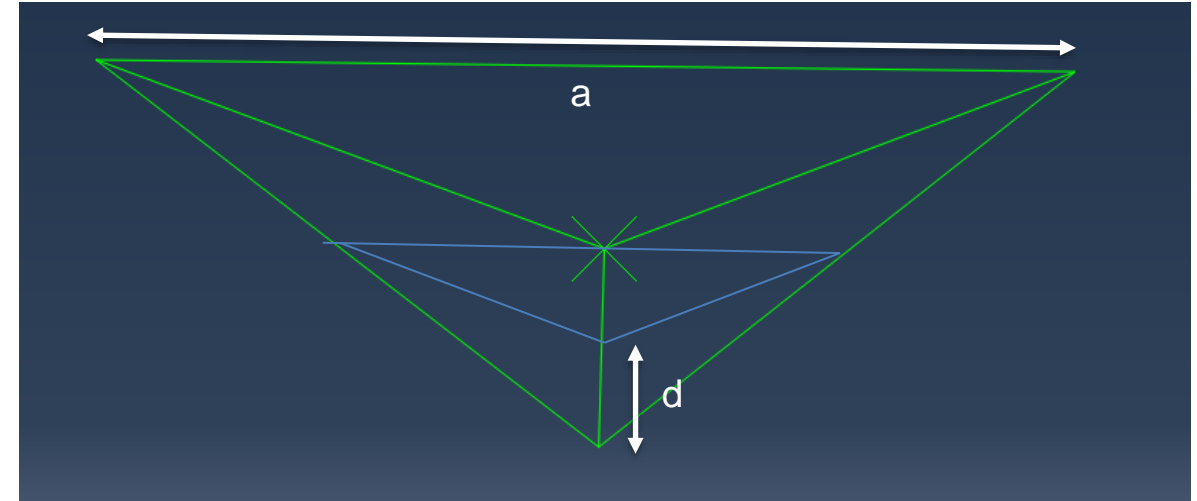
**Table 1.** Mechanical and thermal properties of the modelled material

Density (kg/m <sup>3</sup> )	Thermal conductivity (W/(m·K))	Elastic modulus (GPa)	Poisson's ratio	Yield stress (MPa)
8.96e3	386	115	0.34	33.3



# Calculations

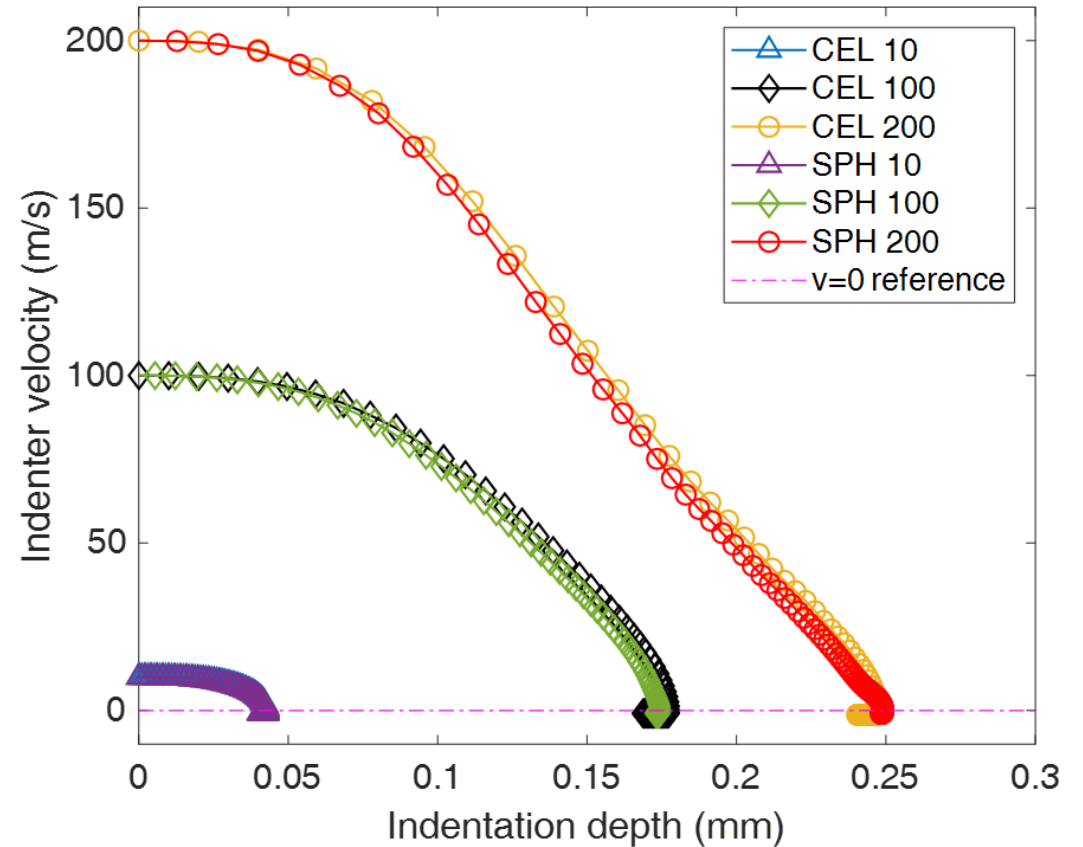
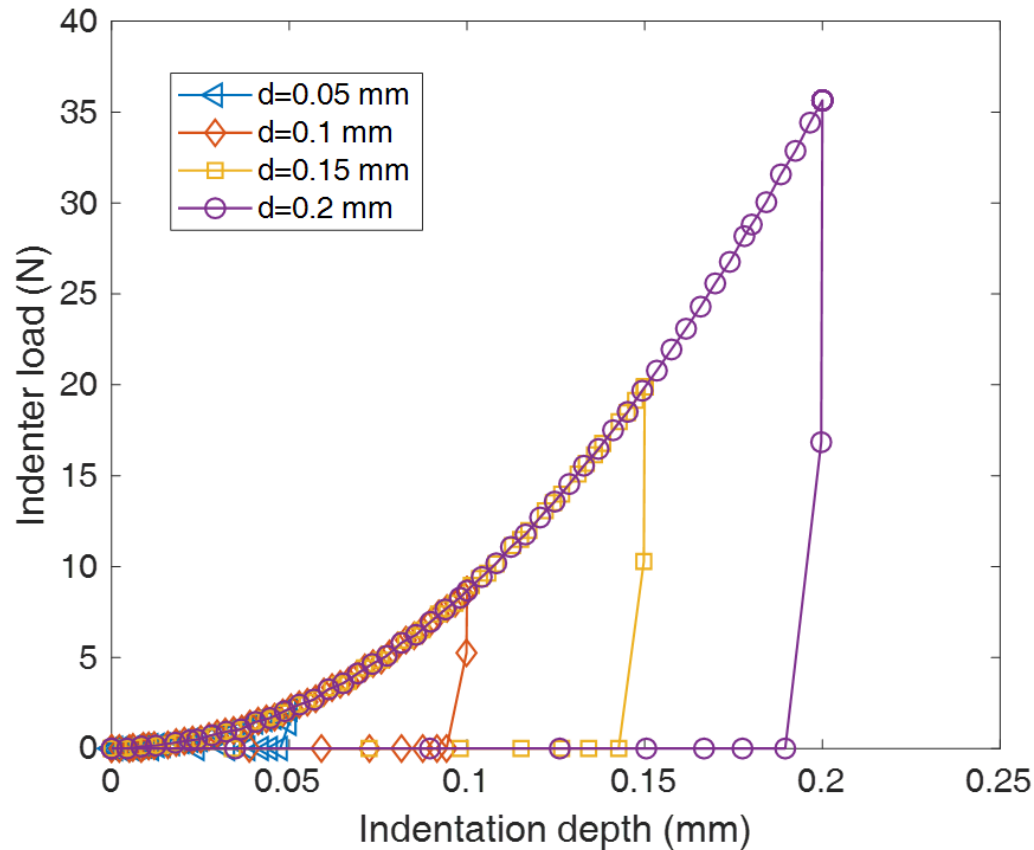
- $H_d = \frac{\int F_{load} dx - \int F_{unload} dx}{V_{indentation}}$ , for static indentation
- $H_d = \frac{0.5 \cdot m_i \cdot (v_i^2 - v_r^2)}{V_{indentation}}$ , for dynamic projectile
- $R_H = \frac{H_d}{\sigma_0}$



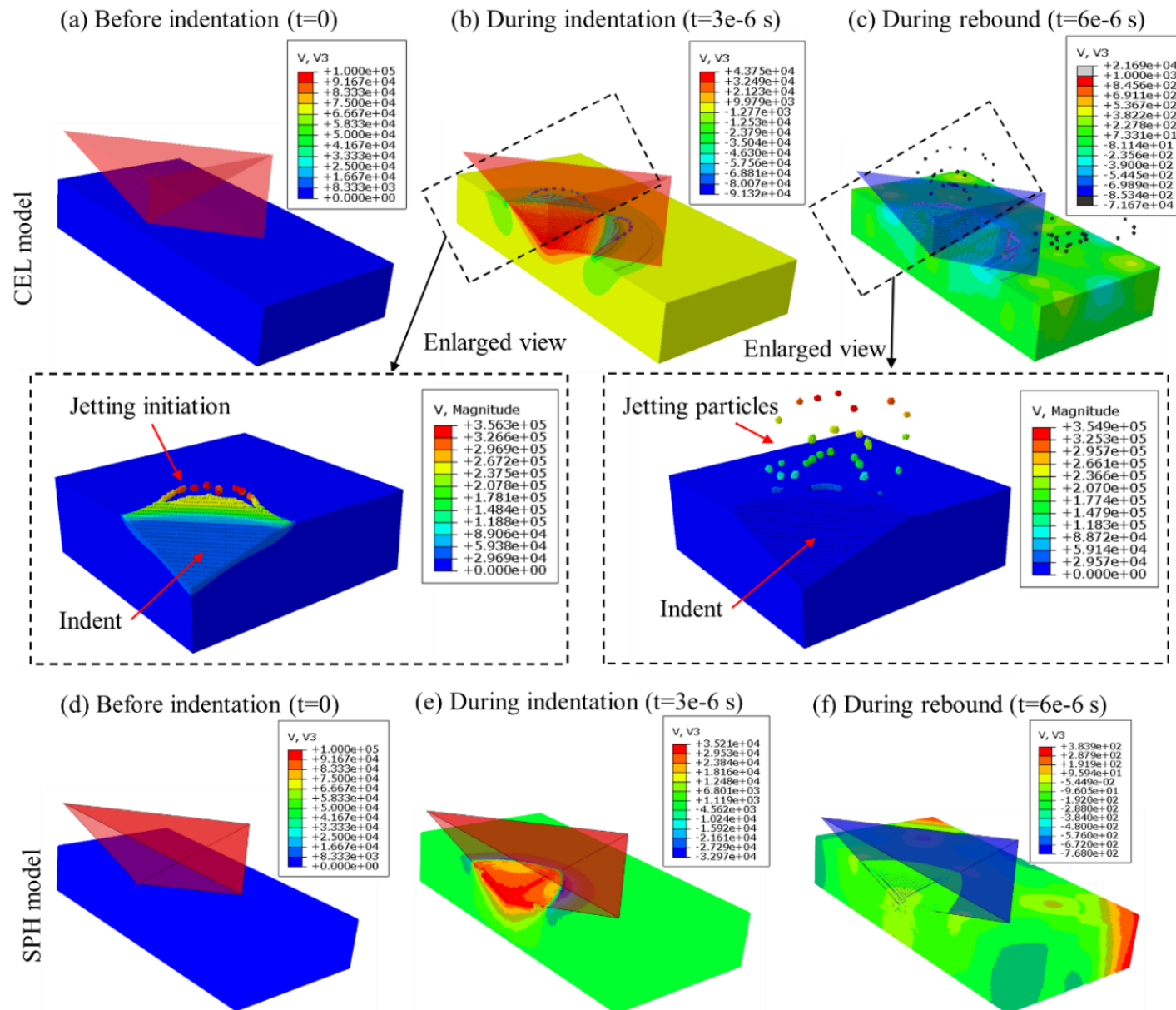
a (mm)	0.02	0.2	2
vi (m/s)	50	10	50
	100	50	100
		100	
	200	150	200
		200	



# Results: static indentation and dynamic projectile

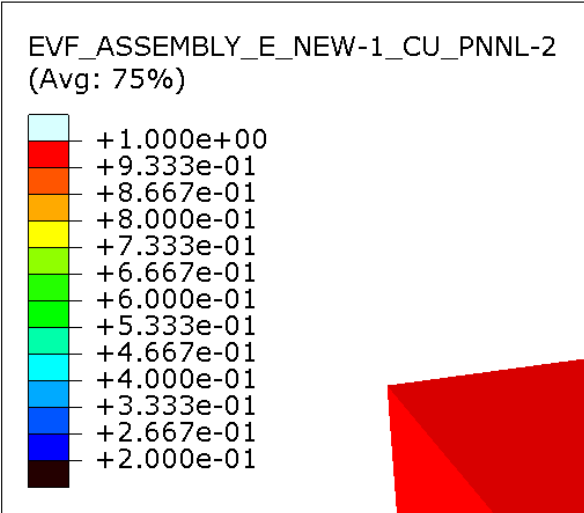


# Results: CEL vs SPH

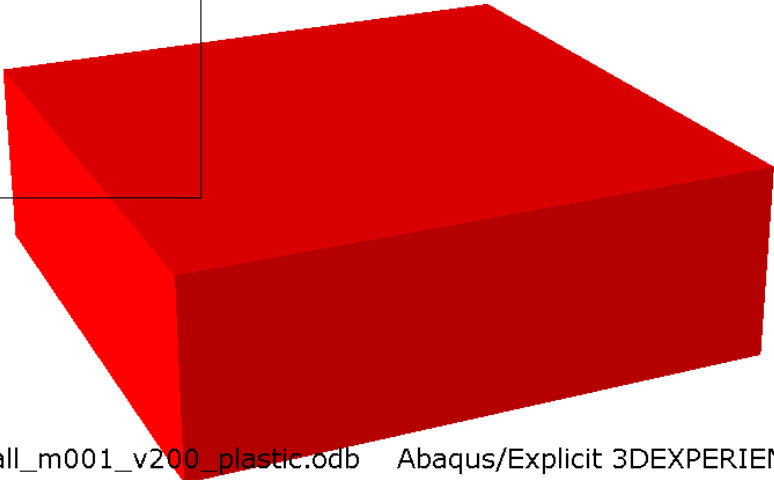




# CEL shows jetting



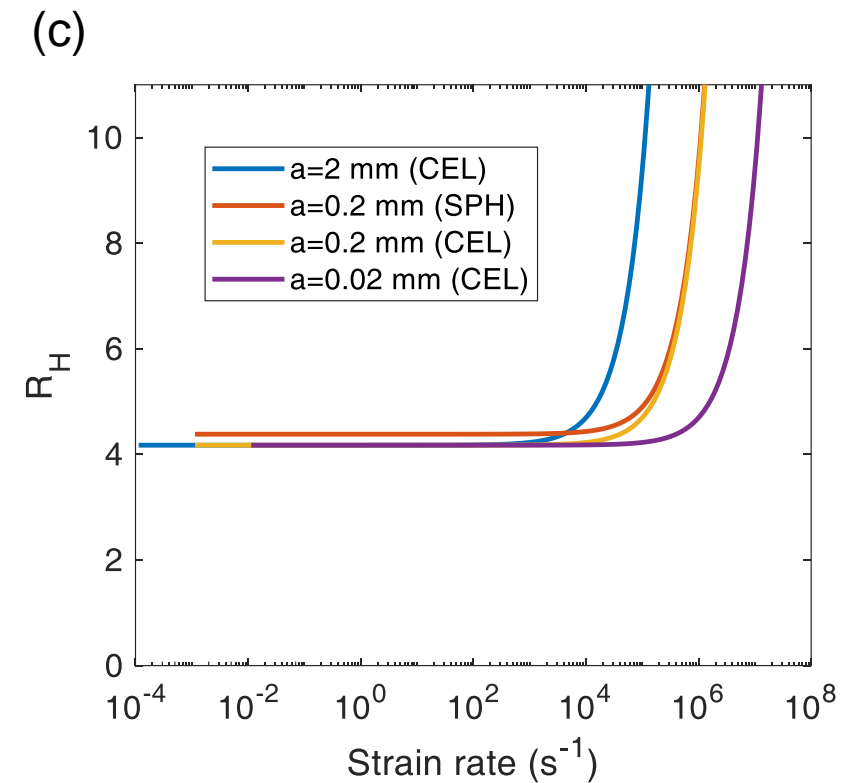
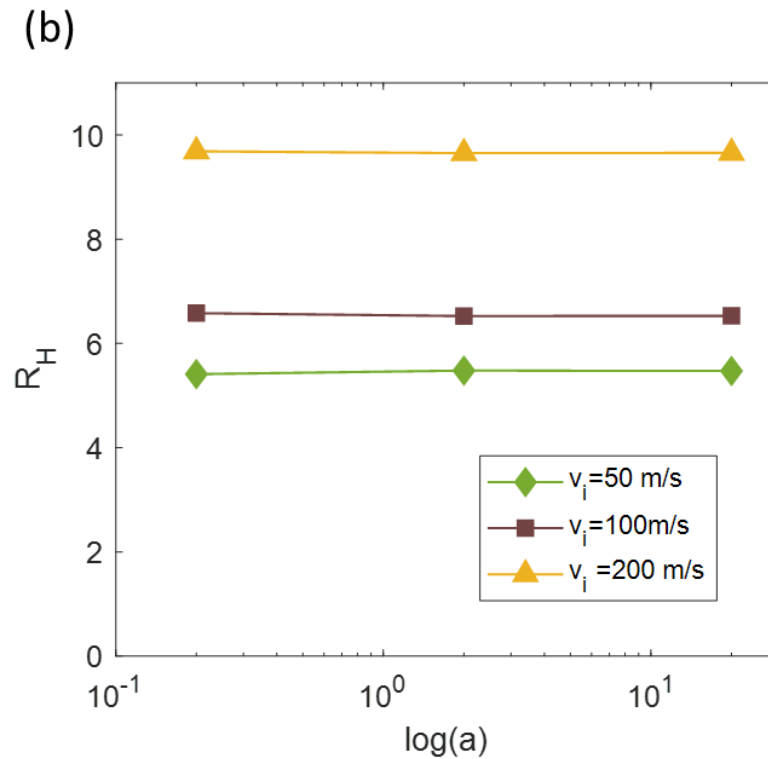
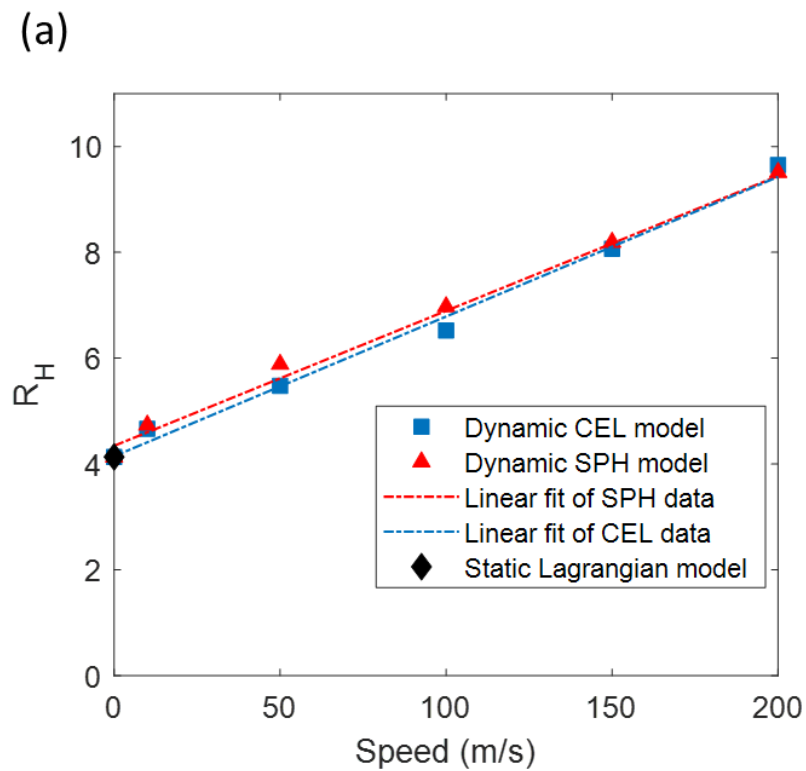
Step: Step-1 Frame: 0  
Total Time: 0.000000



$V_i = 200 \text{ m/s}$

ODB: CEL\_small\_m001\_v200\_plastic.odb Abaqus/Explicit 3DEXPERIENCE R2018x Tue Jul 21 0  
Step: Step-1  
Increment 0: Step Time = 0.0  
Primary Var: EVF\_ASSEMBLY\_E\_NEW-1\_CU\_PNNL-2  
Deformed Var: U Deformation Scale Factor: +1.000e+00

# Dynamic hardness: roles of strain rate vs speed

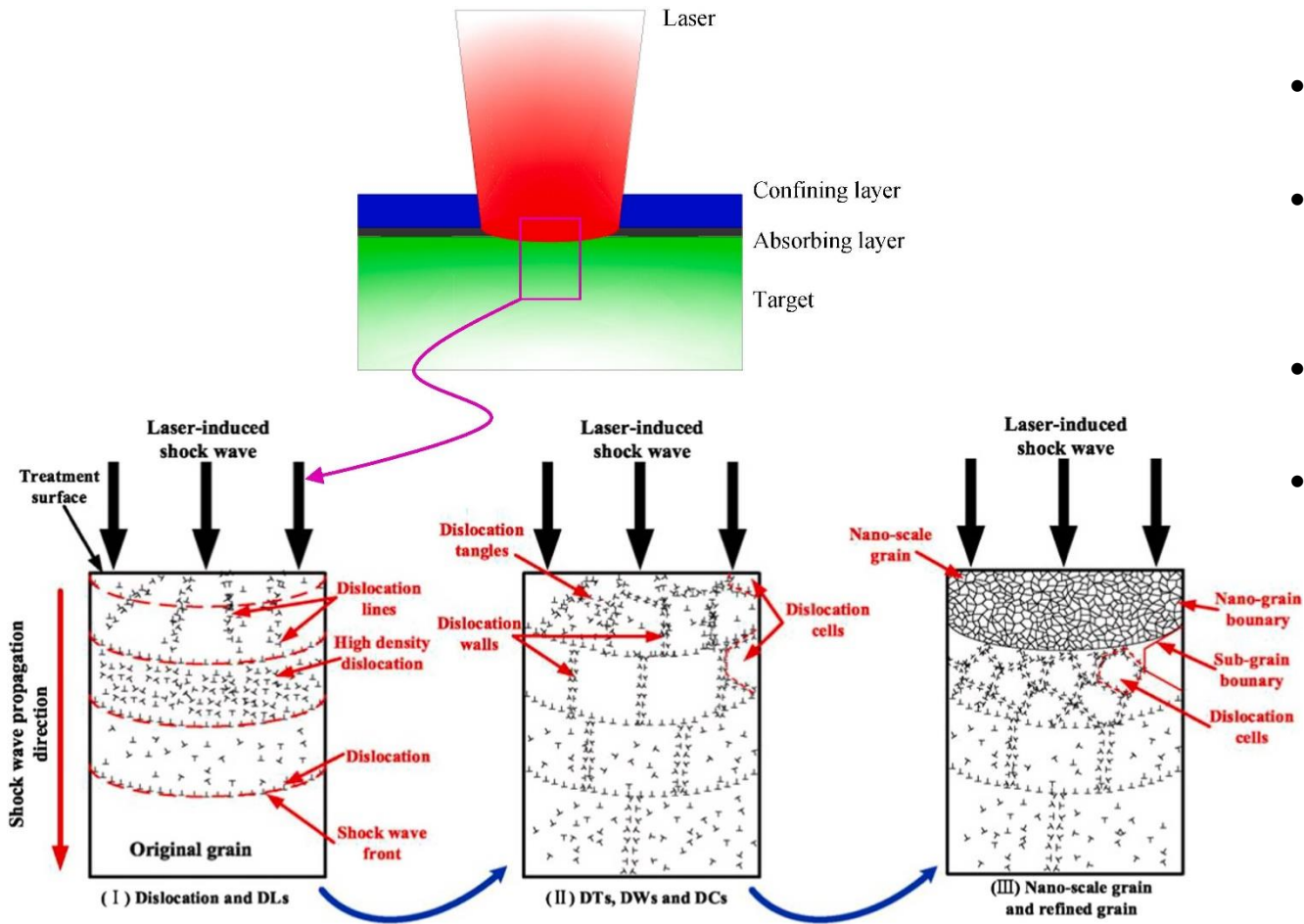


- Dynamic hardness increases with impact speed instead of strain rate

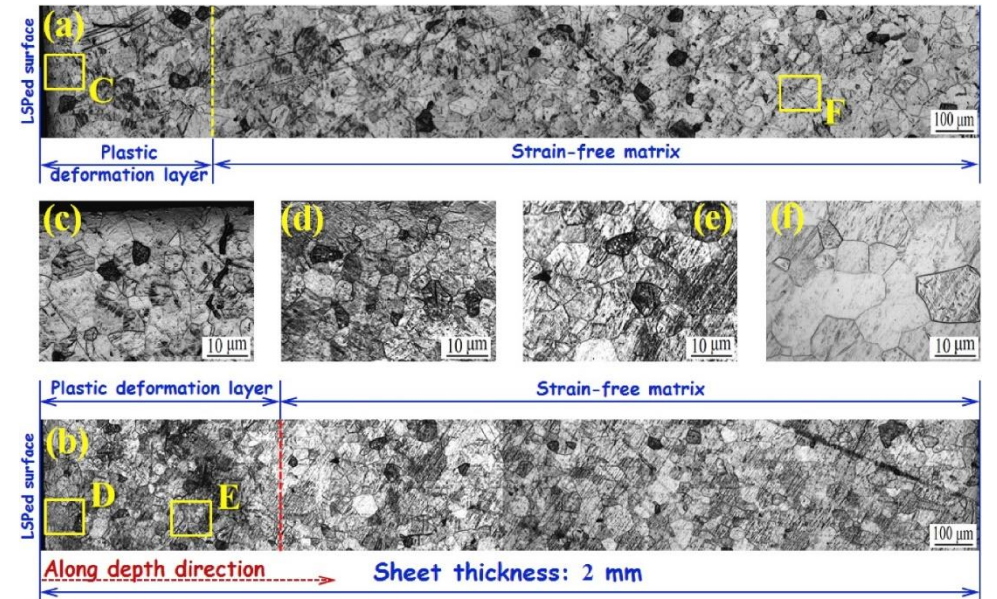


# Shock-hardening in laser shock peening (LSP)

- LSP: Shock pressure of 15-20 GPa (Wang et al., 2020) under uniaxial strain state.
- $v_i = 750\text{m/s}$  generates 16.7 GPa impact between the alumina particle and Cu plate (Hugoniot calculation)
- The shock front induces grain refinement, causing hardening.
- This process may not involve strain-rate hardening.



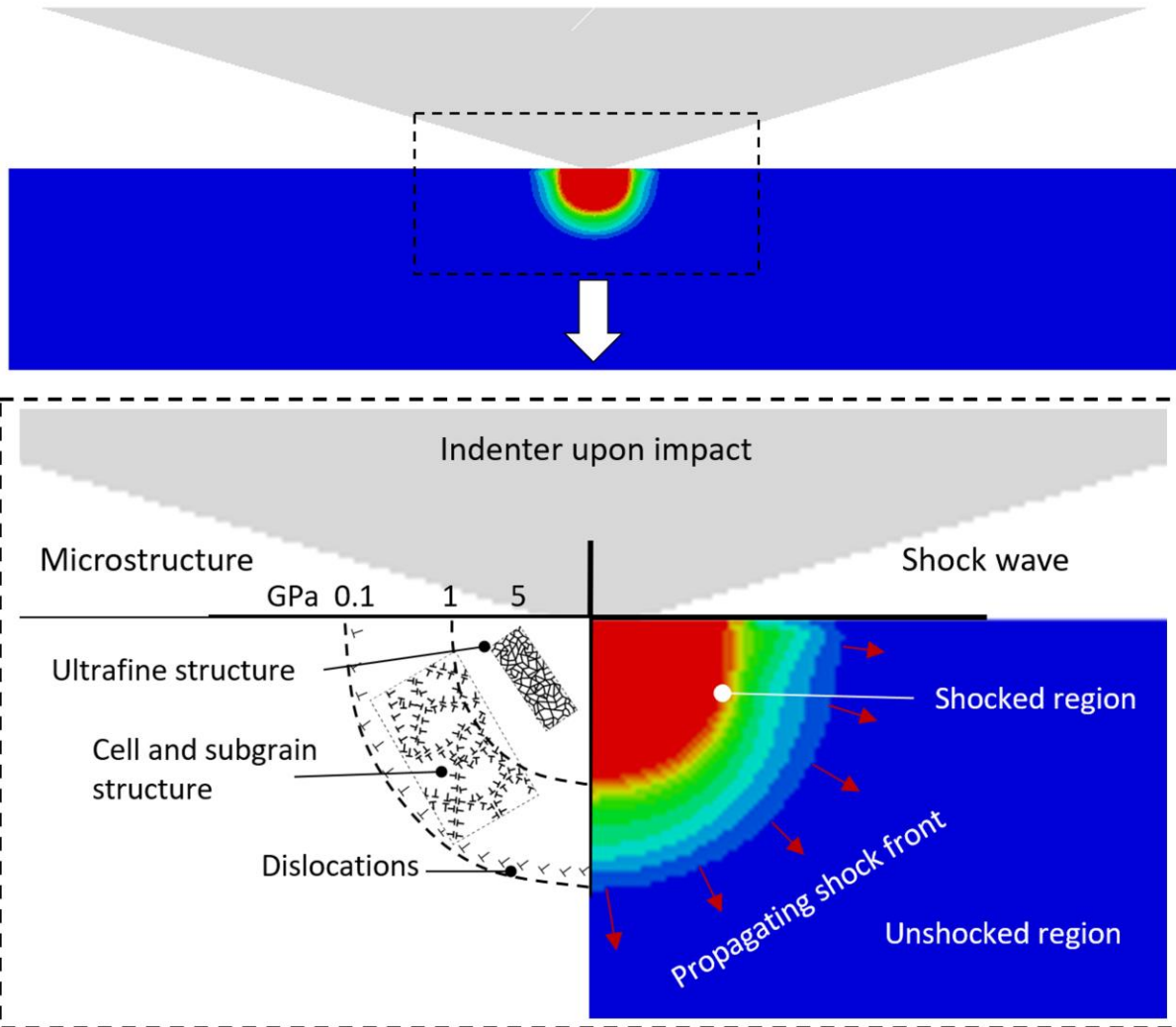
Wang et al. (2020)



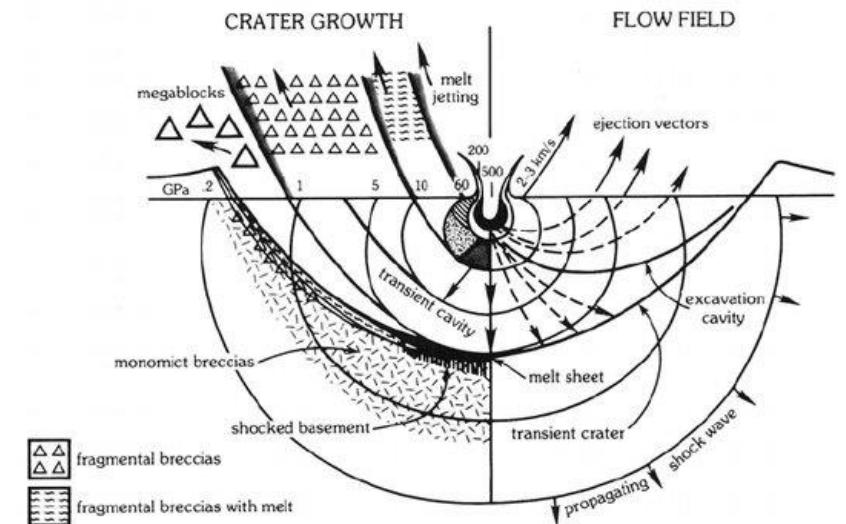
Lu et al. (2017)



# Shock propagation



- Shock front moves much faster than the particle or indentation-driven displacement. ( $v_s=4.72$  km/s, for ceramic-copper impact  $v_i=750$  m/s)
- A discrete uniaxial-strain interface is created between the shocked and unshocked regions.
- Dislocations are generated from elastic distortion and pinched out at the shock front.
- Significant microstructural hardening ahead of the larger displacements required to accommodate the indenter.



Stöffler et al. (2007)



# Summary and future work

- Without rate-hardening model, a clear linear speed effect with no size effect on dynamic energetic hardness is observed.
- Shock effects can induce unique microstructures and significant hardening.
- Shock hardening has different origins and phenomenology than strain rate hardening. A complete model needs to be established:
  - a quantitative model to show the effects of density and modulus on the slope of the H-vi curve.
  - an analytical model to understand the origin of the behavior

